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(71) Applicant: SOCIETE DES PRODUITS NESTLE S.A. 1800 Vevey (CH)

(72) Inventors:

 Haefliger, Hanspeter 8400 Winterthur (CH) Berg, Udo
 61184 Karben (DE)

Germeroth, Hans-Wilhelm
 61118 Bad Vilbel (DE)

 Schuster, Volkmar 61350 Bad Homburg (DE)

Kehrli, Peter
 8404 Winterthur (CH)

(74) Representative:
Wavre, Claude-Alain et al
55, avenue Nestlé
1800 Vevey (CH)

(54) Granular baking improver product

(57) A granular baking improver product, which has a mean particle diameter of from 300 to 500 μ m, less than 1% by volume of the particles having a diameter smaller than 50 μ m, and a process for the production of such a granular baking improver product, which consists of preparing a premix of powdered constituents and forming the premix into granules or agglomerates by continuously dispersing liquid malt extract and liquid emulsifier into a flow of the premix.

Description

[0001] The present invention relates to a granular baking improver product and to a process for the production of a granular baking improver product.

[0002] Bread baking improvers are used for the dough preparation in bakeries, in order to better control the baking properties of the flour, and to regulate enzyme activity. Bread baking improvers traditionally contain emulsifiers and malt components, generally in powder form. Although the emulsifiers are diluted with flours, the powder may lump or even block in the bag, especially by increasing temperature. In addition, very fine powder particles below about 50 µm are considered as dust which can cause allergies like the typical baker-asthma (occupational asthma).

[0003] EP0650669 (GIST-BROCADES) discloses a baking improver composition in a homogeneous solid shaped form comprising one or more baking improver agent and a binding agent which permits disintegration of the solid form when in use for mixing a dough. The solid shaped form may be capable of manual division into smaller dosage units and may be obtained by compacting a powder composition based on flour and containing about 20 to 30% by weight of lecithin as a binding agent and baking emusifier, for example.

[0004] WO9501727 (QUEST INTERNATIONAL) discloses enzymes which are in a particulate, non-dusting form and which are substantially non-allergenic. The particles comprise a binding agent which is substantially insoluble in water, especially a binding agent consisting of at least 50% of an emulsifier, the enzymes being dispersed therein and being released upon the application of shear forces, especially during kneading or extruding a food mixture, for example.

20 [0005] The particles may be obtained by spray chilling a liquid mixture of enzyme solution and molten emulsifier.

[0006] DE19708165 (HENKEL) discloses a process for manufacturing a granular baking aid by extrusion, which consists of simultaneously mixing and extruding practically anhydrous baking aid constituents, in order to avoid adding water at the beginning and drying in the end of the manufacturing process.

[0007] A first object of the present invention is to provide a granular baking improver product which is not dusting, which is free flowing, which offers resistance to compactation and which is easy to be broken after compactation.

[0008] A second object of the present invention is to provide a process for the production of a granular baking improver product which permits the use of liquid malt and liquid emulsifier for granulating and/or agglomerating powdered constituents of the baking improver.

[0009] It has now been found that the first object of the present invention can be met by a granular baking improver product, which has a mean particle diameter of from 300 to 500 μ m, less than 1% by volume of the particles having a diameter smaller than 50 μ m, which comprises, in % by weight, from 8 to 20% of malt extract and/or high melting fat, from 8 to 20% of emulsifier, from 15 to 25% of stabiliser, from 45 to 69% of filler, up to 4% of enzyme mix, up to 5% of acid and up to 0.5% of oxidising agent, and which has a moisture content of from 4 to 6%.

[0010] It has been found that the second object of the present invention can be met by a process for the production of a granular baking improver product which consists of preparing a premix of powdered constituents comprising, in % by total weight of premix plus liquids, from 15 to 25% of stabiliser, from 45 to 69% of filler, up to 4% of enzyme mix, up to 0.5% of acid and up to 0.5% of oxidising agent, and forming the premix into granules or agglomerates by continuously dispersing liquids comprising from 8 to 20% of liquid malt extract and/or high melting fat, from 8 to 20% of liquid emulsifier and up to 5% lactic acid into a flow of the premix.

[0011] The outstanding properties of the present granular baking improver product, in so far as it is not dusting, it is free flowing, it offers resistance to compactation and it is easy to be broken after compactation, may be checked and defined by means of particle size analysis, compactation test and compression strength test as described later on, for example.

[0012] Furthermore it was found that the present granular baking improver product may disintegrate so fast in a dough kneading process that there is no difference as compared with a traditional powdered product in this respect.

[0013] In addition, the fact that liquid malt and liquid emulsifier may be used in the present process for the production of a granular baking improver product indeed appears to be advantageous both with regard to appreciable cost savings regarding the raw material to be used and with respect to the outstanding properties of the granular product thus obtained.

[0014] A further advantage of the present process is that it may not be necessary to postdry the present product after it has been formed into granules or agglomerates.

[0015] Thus, the present granular baking improver product has a mean particle diameter of from 300 to 500 μ m, less than 1% by volume of the particles having a diameter smaller than 50 μ m.

[0016] Preferably, at least 90% by volume of the particles have a diameter of 100 µm or more and the particles have a span in diameter distribution of from 1.5 to 2.5.

[0017] The span is defined as the broadness or width in particle distribution between a 10% limit and a 90% limit divided by the mean particle diameter, whereby 10% by volume of the particles have a diameter below the 10% limit and 90% by volume of the particles have a diameter below the 90% limit.



[0018] The present granular baking improver product comprises, in % by weight, from 8 to 20% of malt extract and/or high melting fat, from 8 to 20% of emulsifier, from 15 to 25% of stabiliser, from 45 to 69% of filler, up to 4% of enzyme mix, up to 5% of acid and up to 0.5% of oxidising agent.

[0019] The expression "high melting fat" means a fat having a melting temperature above ambient temperature.

[0020] The high melting fat preferably has a melting temperature of from 45 to 60°C and it may be a vegetable fat such as palm fat, for example.

[0021] The emulsifier may be a lecithin, a mono- or diglyceride of fatty acid, a calciumstearoyllactylate, a sodium stearoyllactylate, a polysorbate and/or a datem (mono- and diacetyl tartaric acid ester used for bakery products), for example.

[0022] The stabiliser may be guar gum, xanthan, locust bean gum, carboxymethylcellulose, alginate, pregelatinised flour, especially pregelatinised wheat or corn flour, and/or acidic calcium pyrophosphate, for example.

[0023] The filler may be sugars such as sucrose, dextrose or lactose, maltodextrin, wheat flour, malt flour, buttermilk powder, wheat gluten, starch (potato, wheat, corn), calciumsulfate, calciumcarbonate, tricalciumphosphate and/or soya flour, for example.

[0024] The enzyme mix may comprise any food grade amylase, hemicellulase, lipase and/or protease, for example.

[0025] The acid may be citric acid, lactic acid, acetic acid or tartaric acid, for example.

[0026] The oxidising agent may be ascorbic acid, L-cystein or cystine, for example.

[0027] As stated above, the present process for the production of a granular baking improver product consists of preparing a premix of powdered constituents comprising, in % by total weight of premix plus liquids, from 15 to 25% of stabiliser, from 45 to 69% of filler, up to 4% of enzyme mix, up to 0.5% of acid and up to 0.5% of oxidising agent, and forming the premix into granules or agglomerates by continuously dispersing liquids comprising from 8 to 20% of liquid malt extract and/or high melting fat, from 8 to 20% of liquid emulsifier and up to 5% lactic acid into a flow of the premix.

[0028] In addition to what has been said above as to what the different constituents may be or preferably are, it may be stated here that the powdered filler also may comprise a part of malt in dried form, for example.

[0029] The liquid mait extract may have a moisture content of from 15 to 25%, for example.

[0030] The high melting fat may be heated to a temperature above its melting point in order to be in liquid form.

[0031] The emulsifier may be heated to a temperature above its melting point in order to be in liquid form.

[0032] Preparing the premix may be carried out by means of any suitable traditional powder mixer such as a horizontal mixer with plow-shaped heads arranged on its horizontal shaft or a ribbon mixer, for example.

[0033] Forming the premix into granules or agglomerates by continuously dispersing the liquids into a flow of the premix may be carried out by means of one or more injection nozzles provided for injecting the liquids into a flow of the premix, and by means of an agitator provided for creating a highly turbulent flow of premix within a mixing space or chamber into which the liquids are injected, for example.

[0034] The injection nozzles may comprise a cylindrical conduct having a circular opening positioned beneath or within the flow of premix, for example.

[0035] The agitator may comprise agitating means such as paddles or knifes arranged around a rotating shaft capable of high rotation speed of from about 800 to 3000 rotation per min (rpm), for example.

[0036] The liquids may be injected into the flow of premix separately, or after having been intimately and continuously mixed together beforehand by passing through a static mixer, for example.

[0037] A continuous high speed ring layer granulator may be used for forming the premix with the liquids into granules, for example. Such granulator consists of a rotating agitator and a cylindrical housing. The agitator comprises a large number of flat paddles with adjustable pitch arranged around a horizontal rotating shaft, which sweep close to the inner surface of the housing.

[0038] A flow of premix introduced at ambient temperature into the granulator may be formed into a rather thin ring layer of from about 2 to 10 mm in thickness, flowing close to the inner surface of the housing, for example. The liquids may be injected into the thin ring layer at a temperature of from 45 to 70°C, through injection nozzles having their injection openings positioned beneath or even within the layer, for example. High paddle or rotor speed, preferably a speed of from 800 to 3000 rpm, may create a high turbulence in the thin ring layer, continuously exposing new particle surfaces to the liquid for a rather short residence time of from about 2 to 10 s influenced by the rotor speed and the pitch of the paddles, for example.

[0039] A vertical agglomerator may be used for forming the premix with the liquids into agglomerates, for example. Such agglomerator consists of a vertical agitator with mixing knifes arranged around a vertical shaft which rotates within a mixing chamber defined by a flexible rubber tube.

[0040] In such agglomerator the powdered premix passes through the mixing chamber in a downward flow and the mixing knifes may cause severe turbulences by rotating at a high speed of from 800 to 3000 rpm, for example. The liquids may be injected at the top of the mixing chamber through binary nozzles downwards into the flow of premix. The injected liquids and the powdered premix move down the mixing chamber in a spiral path for a residence time which is influenced by the angle and speed of the mixing knifes and which may be of from 2 to 10 s, for example.

[0041] Embodiments of the granular baking improver product and of the process for producing it according to the present invention are illustrated in the following Examples in which the percentages are by weight unless indicated to the contrary.

[0042] The Examples are preceded by a short description of methods used for defining some of the properties of the granular baking improver product thus obtained.

Method 1: Particle size analysis

[0043] The particle size of the granular product was measured by means of a laser diffraction particle sizer (MASTERSIZER S, Malvern Instruments Ltd., Malvern/GB), coupled with a fully automated, air pressure controlled dry powder feeder (GMP ultra).

[0044] The result from the analysis was the relative distribution of volume of the particles in the range of size classes. Cumulative undersize curves and the following particle size distribution parameters were derived from these basic results:

D50: 50% limit = mean particle diameter (50% by volume of the particles had a diameter below D50 and 50% by volume of the particles had a diameter above D50).

D01: 1% limit (1% by volume of the particles had a diameter below D01)

D10: 10% limit (10% by volume of the particles had a diameter below D10)

D90: 90% limit (90% by volume of the particles had a diameter below D90)

Span: (D90-D10)/D50

Method 2: Flowability

[0045]

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W: angle of repose (°) cot: cotangent to angle of repose (-)

Method 3: Compactation test

[0046] A standardised product sample (present granular product or comparative powdered product) in tablet form (49x29x24 mm) was compacted by a uniaxial solidifying tension force. The applied compactation force of 16870 N corresponds to the surface pressure of 1200 kg / Palette of 80x120 cm and hence simulated actual storage conditions for bread improver.

[0047] The increase in bulk density within the compacted sample and the penetration depth of the piston in the product tablet were used for appreciating flowing properties, that means the flow behaviour deteriorates by increasing penetration depth or density.

Method 4: Compression strength test

[0048] The compacted product tablets (see Method 3) were exposed to a vertical crushing stress. A timely increasing crushing tension leads to tablet breaking, thereby indicating a "resistance to rupture" or "liquid-flow" limit of the tension leads to tablet breaking, thereby indicating a "resistance to rupture" or "liquid-flow" limit of the compacted product. The maximum force at breaking was recorded.

[0049] The lower the crushing tension required for breaking the tablet, the better the flowing properties of the bulk material.

Comparisons

55 [0050] A powdered baking improver product available on the German market was used for comparing properties of the present granular product with corresponding properties of an existing powdered product.

Example 1

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[0051] A granular baking improver product was produced by means of an equipment comprising a RMG 30 type RUBERG continuous high speed ring layer granulator.

[0052] To this end a powdered premix was prepared in a horizontal mixer with plow-shaped heads arranged on its horizontal shaft, which had the following composition, in % of the total weight of premix plus liquids:

Crystal sugar (sucrose)	17.95
Emusifier E 471	1.80
Soya flour	4.90
Guar gum	17.00
Ascorbic acid	0.20
Enzyme mix	2.50
Acidic calcium pyrophosphate	2.10
Dextrose	7.30
Wheat flour	18.55

[0053] The premix had a water content of 3.2%.

[0054] 9.05% of a liquid malt extract (water content 21.4%; malt content 100% on dry matter) and 10.5% of an emulsifier (mono- and diacetyl tartaric acid ester) were heated to 50°C and intimately mixed by passing through a static mixer.

[0055] The powdered premix was passed through the granulator at a flow rate of about 600 kg/h. The rotor speed was of about 2400 rpm, the thickness of the ring layer was of about 3 to 4 mm and the residence time was of about 5 s.

[0056] Simultaneously the liquids were injected into the ring layer of powdered premix through an injecting nozzle positioned near the entry of powder premix into the granulator.

[0057] The granular baking improver product thus produced was collected at the outlet of the granulator, cooled down to ambient temperature and packaged into plastic bags. It had the properties indicated in table 1 hereafter:

Table 1

Parameter	Granular product Example 1	Comparison (powdered product)
D01 (μm)	60	7
D10 (μm)	128	20
D50 (μm)	356	98
D90 (μm)	979	1199
Span (-)	2.39	12.03
Compactation depth (mm)	0.53	0.72
Breaking force (N)	3.4	5.3
Flowability W (°)	41.3	52.4
Flowability cot (-)	1.14	0.77

Table 1 illustrates clearly the fact that the particle size distribution of the present granular product is much better defined than the one of the known powdered product and that, contrarily to the known powdered product, the present product is not dusting (D01 of 60 μm as compared with 7 μm), it offers a relatively good resistance to compactation, it is relatively easy to be broken after compactation and it has a good flowability (cot value of 1.14 as compared



with 0.77, taking the fact into consideration that the flowability may be considered to be good as soon as the cot value is at least 1.0).

Example 2

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[0059] A granular baking improver product was produced by means of an equipment comprising a Flexomix type SHUGI agglomerator.

[0060] To this end a powdered premix was prepared in a horizontal mixer with plow-shaped heads arranged on its horizontal shaft, which had the following composition, in % of the total weight of premix plus liquids (without added tap water):

Ground sugar (sucrose)	42.00
Emusifier E 471	3.60
Soya flour	4.35
Guar gum	16.10
Ascorbic acid	0.18
Enzyme mix	2.80
Wheat flour	7.97
Fat/Lecithin	2.50

[0061] 12.0% of a liquid malt extract (water content 21.4%; malt content 100% on dry matter), 8.5% of an emulsifier (mono- and diacetyl tartaric acid ester) and tap water (about 20% by weight of the total liquid mixture) were mixed in a tank and heated to about 50°C.

[0062] The powdered premix was passed downwardly through the agglomerator at a flow rate of about 450 kg/h, the residence time being of about 3 s. The shaft rotating speed was of about 3000 rpm.

[0063] Simultaneously the liquid mixture was injected or sprayed downwardly into the flow of powdered premix into the mixing chamber through binary injecting or spraying nozzles positioned on the top of the mixing chamber.

[0064] The granular baking improver product thus produced was collected at the bottom of the agglomerator, fluid bed dried to a residual water content of about 6%, cooled down to ambient temperature and packaged into plastic bags. It had the properties indicated in table 2 hereafter:

Table 2

Parameter	Granular product Exam- ple 1	Granular product Exam- ple 2	Comparison (powdered product)
D01 (μm)	60	80 .	7
D10 (μm)	128	187	20
D50 (µm)	356	450	98
D90 (μm)	979	1031	1199
Span (-)	2.39	1.88	12.03
Compactation depth (mm)	0.53	0.3	0.72
Breaking force (N)	3.4	0.8	5.3
Flowability W (°)	41.3	39.4·	52.4
Flowability cot (-)	1.14	1.22	0.77

[0065] Table 2 illustrates the fact that the particle size distribution of the present granular product obtained in Example 2 is also much better defined than the one of the known powdered product and that, contrarily to the known powdered product and that, contrarily to the known powdered product and that the particle size distribution of the present granular product obtained in Example 2 is also much better defined than the one of the known powdered product and that, contrarily to the known powdered product and that the particle size distribution of the present granular product obtained in Example 2 is also much better defined than the one of the known powdered product and that, contrarily to the known powdered product and that the particle size distribution of the present granular product obtained in Example 2 is also much better defined than the one of the known powdered product and that, contrarily to the known powdered product and that the particle size of the present granular product obtained than the one of the known powdered product and that the particle size of the known powdered product and that the particle size of the present granular product and that the particle size of the present granular product obtained the particle size of the present granular product obtained the present granular product obtained the present granular product granular gr

dered product, the present product obtained in Example 2 is not dusting (D01 of 80 μ m as compared with 7 μ m), it offers a relatively good resistance to compactation, it is relatively easy to be broken after compactation and it has a good flowability (cot value of 1.22 as compared with 0.77, taking the fact into consideration that the flowability may be considered to be good as soon as the cot value is at least 1.0).

Claims

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- A granular baking improver product, which has a mean particle diameter of from 300 to 500 μm, less than 1% by volume of the particles having a diameter smaller than 50 μm, which comprises, in % by weight, from 8 to 20% of malt extract and/or high melting fat, from 8 to 20% of emulsifier, from 15 to 25% of stabiliser, from 45 to 69% of filler, up to 4% of enzyme mix, up to 0.5% acid and up to 0.5% of oxidising agent, and which has a moisture content of from 4 to 6%.
- A granular baking improver product according to claim 1, in which at least 90% by volume of the particles have a
 diameter of 100 μm or more and the particles have a span in diameter distribution of from 1.5 to 2.5.
 - 3. A process for the production of a granular baking improver product, which consists of preparing a premix of powdered constituents comprising, in % by total weight of premix plus liquids, from 15 to 25% of stabiliser, from 45 to 69% of filler, up to 4% of enzyme mix, up to 0.5% acid and up to 0.5% of oxidising agent, and forming the premix into granules or agglomerates by continuously dispersing liquids comprising from 8 to 20% liquid malt extract and/or high melting fat, from 8 to 20% of liquid emulsifier and up to 5% lactic acid into a flow of the premix.
 - A process according to claim 3, in which the premix is formed into granules within a continuous high speed ring layer granulator consisting of a rotating agitator and a cylindrical housing.
 - 5. A process according to claim 4, in which the agitator rotates at a speed of from 800 to 3000 rpm.
 - A process according to claim 4, in which the liquids are mixed together beforehand by passing through a static mixer.
 - 7. A process according to claim 4, in which the liquids are injected within a thin layer of premix flow having a thickness of from 2 to 10 mm, through one or more nozzles having injection openings positioned within the thin layer of premix



EUROPEAN SEARCH REPORT

Application Number EP 98 20 4169

Category	Citation of document with indica of relevant passages		Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
D,A	DE 197 08 165 A (HENKE (NL)) 3 September 1998 * page 3, line 1-55 * * claim 4 *	1	A23P1/02 A21D6/00 A21D10/00	
A	DE 43 44 107 A (BOEHRI BACKMITTE) 29 June 199 * column 3 * * claims 1,7-21 *		1	
A	US 3 135 612 A (HAIR, LAWRENCE) 2 June 1964 * column 1, line 49 - * column 2, line 42 - * example 3 * * column 3, line 22-41	column 2, line 13 * column 3, line 9 *	1,3,4,6,	
A .	WO 96 03893 A (NESTLE (FR)) 15 February 1996 * page 4, line 33-34 * * claims 1,10 *		1,3	TECHNICAL FIELDS SEARCHED (Int.Cl.6)
Α.	GB 1 168 692 A (OGILVI COMPANY) 29 October 19 * page 2, line 46-56 * * page 2, line 88-110 * page 3, line 90-98 * * claim 1 *	669 : *	3,6,7	A210 A23P
	The present search report has been	drawn up for all claims	_	
-	Place of search	Date of completion of the search		Examiner
	THE HAGUE CATEGORY OF CITED DOCUMENTS ticularly relevant if taken alone	16 April 1999 T: theory or princt; E: earlier patent de after the filing de	ole underlying the locument, but publi	

ANNEX TO THE EUROPEAN SEARCH REPORT ON EUROPEAN PATENT APPLICATION NO.

EP 98 20 4169

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

16-04-1999

	Patent document ed in search repo	rt	Publication date	Patent family member(s)	Publication date
DE	19708165	A	03-09-1998	DE 29719287 U EP 0867116 A EP 0876763 A	26-03-19 30-09-19 11-11-19
DE	4344107	A	29-06-1995	NONE	
US	3135612	A	02-06-1964	NONE	
WO.	9603893	Α	15-02-1996	AU 698226 B AU 3114195 A CA 2196214 A CN 1158075 A EP 0804090 A FI 970326 A JP 10503651 T NO 970348 A NZ 290408 A	29-10-19 04-03-19 15-02-19 27-08-19 05-11-19 27-01-19 07-04-19 06-03-19 26-01-19
GB	1168692	Α	29-10-1969	NONE	

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82